

Assessment on the Stormwater Infrastructure Design Parameter based on the Existing Projects of Sarawak Urban Stormwater Management, SUStoM Facility



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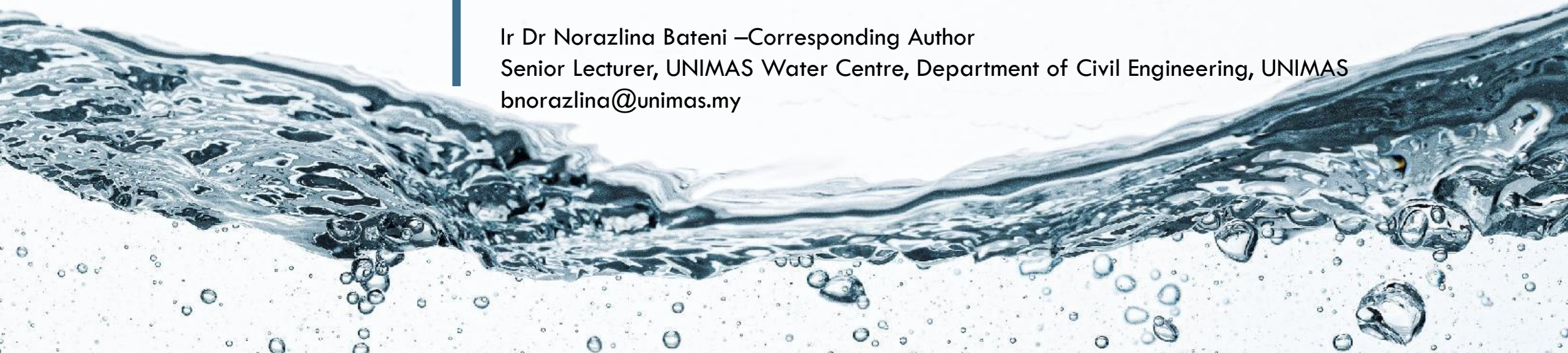
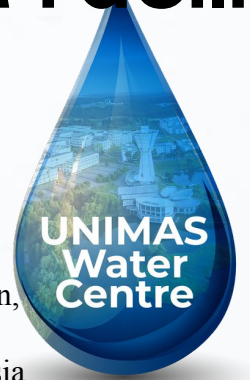
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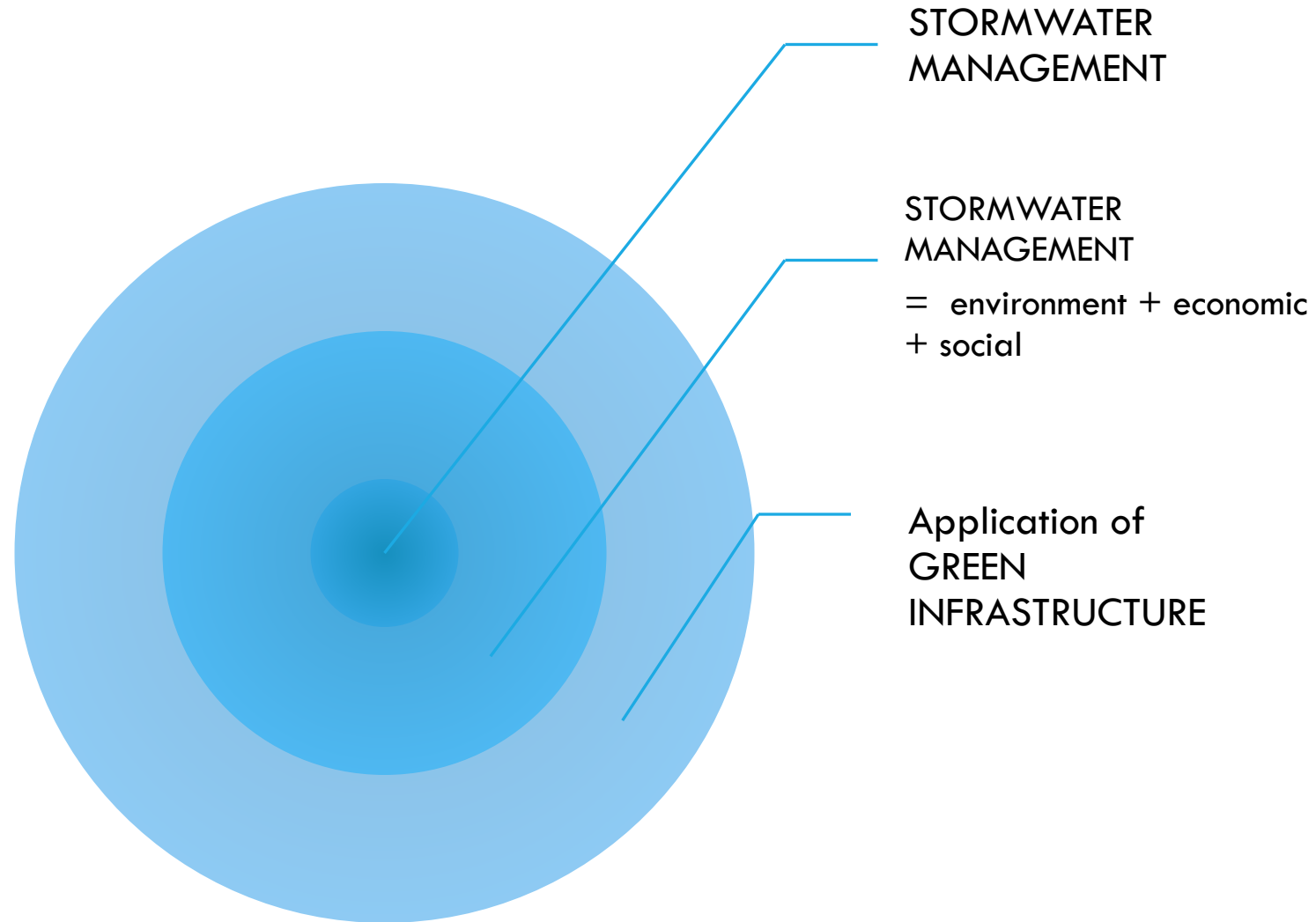
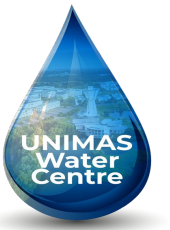
Ir Dr Norazlina Bateni –Corresponding Author

Senior Lecturer, UNIMAS Water Centre, Department of Civil Engineering, UNIMAS

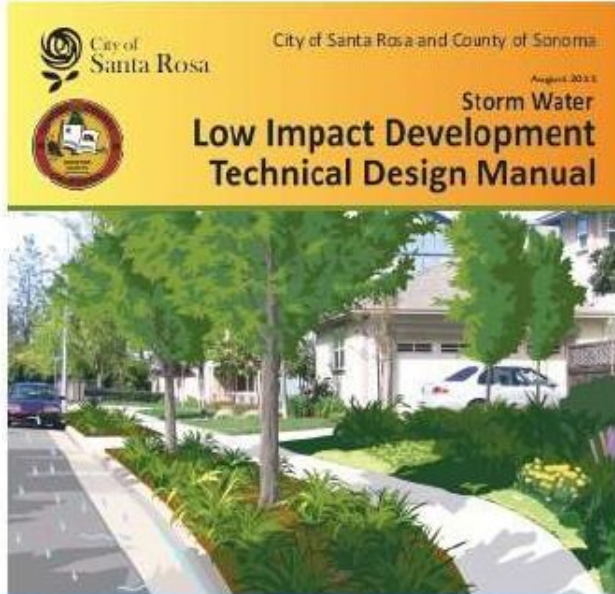
bnorazlina@unimas.my



STORMWATER MANAGEMENT

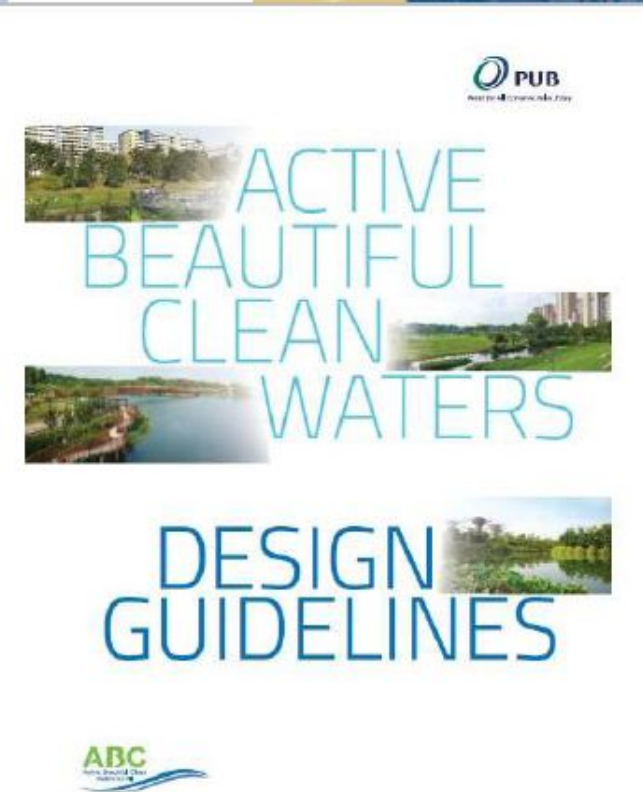
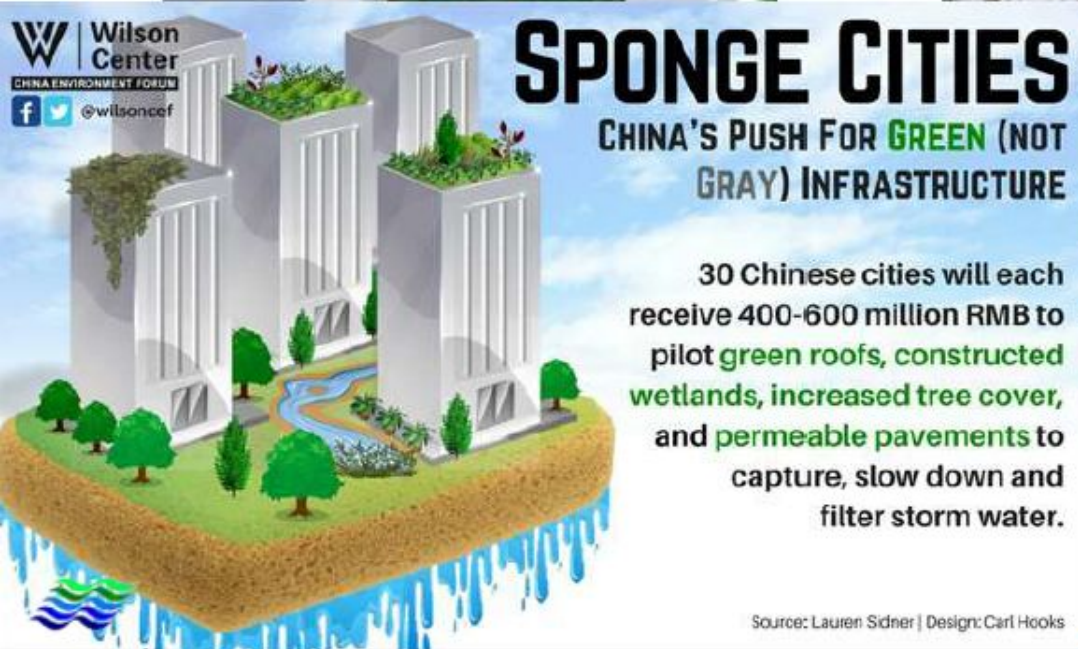


STORMWATER MANAGEMENT/ GREEN INFRASTRUCTURE

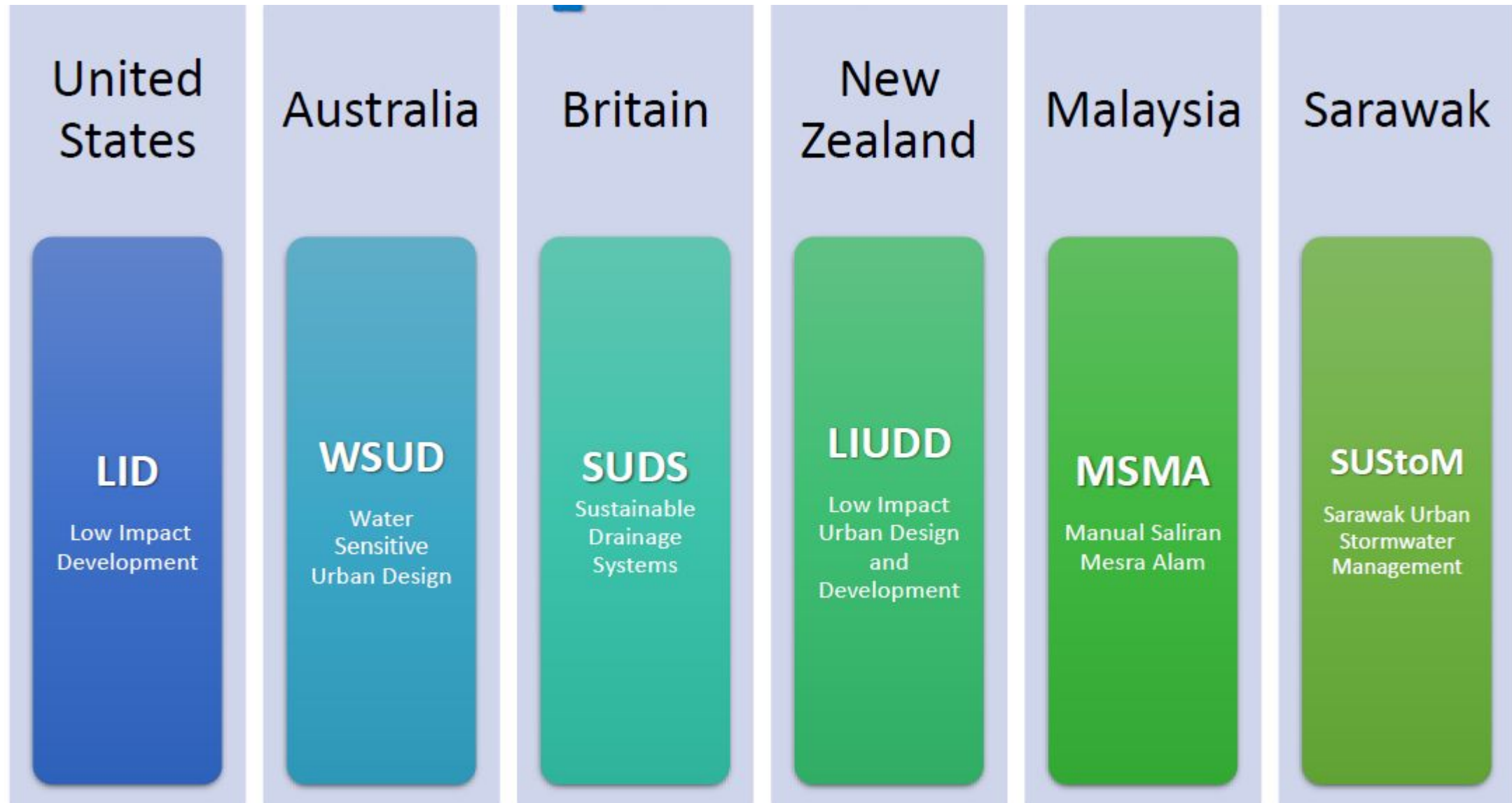


Sustainable Drainage Systems (SUDS)

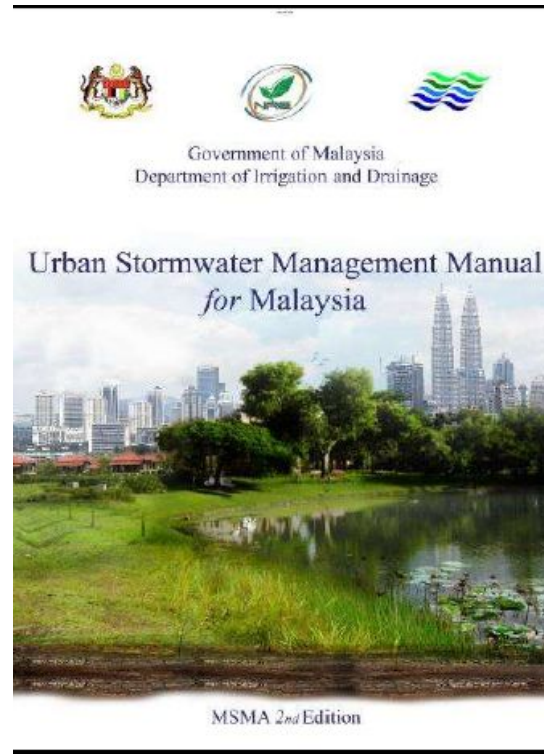
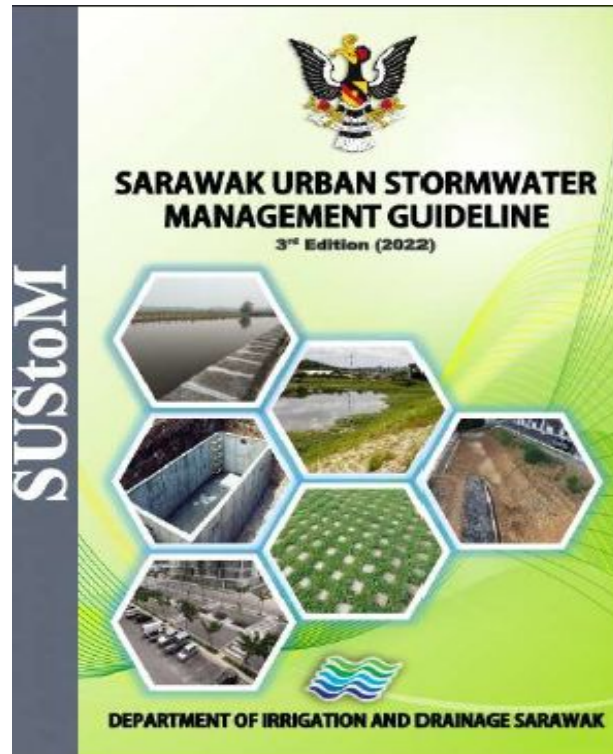
A guide for developers



Stormwater Management/ Green Infrastructure



STORMWATER MANAGEMENT/ GREEN INFRASTRUCTURE

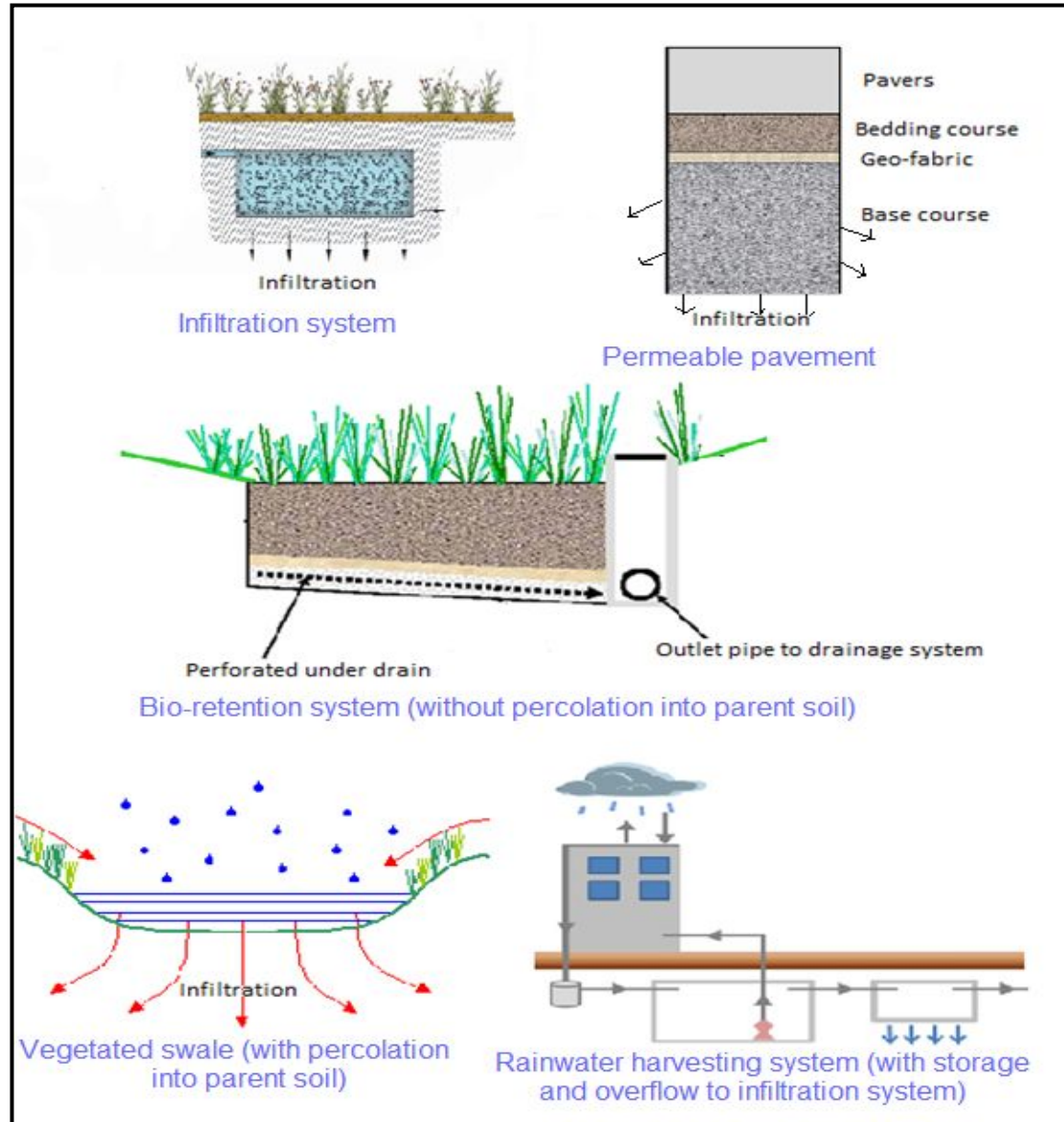


**MANUAL SALIRAN
MESRA ALAM (MSMA)**

**SARAWAK URBAN
STORMWATER
MANAGEMENT
GUIDELINE (SUSToM)**

MSMA/ SUSToM Key Elements





Constructed wetlands

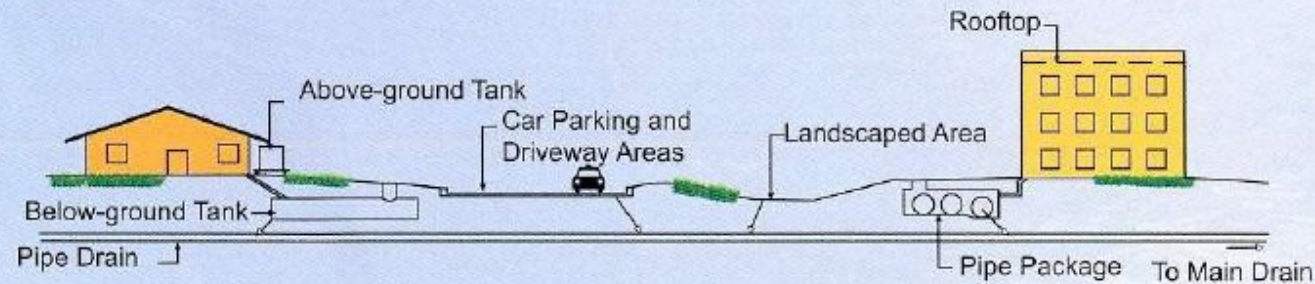


Green roofs

Stormwater Management/ Green Infrastructure



Quantity Control

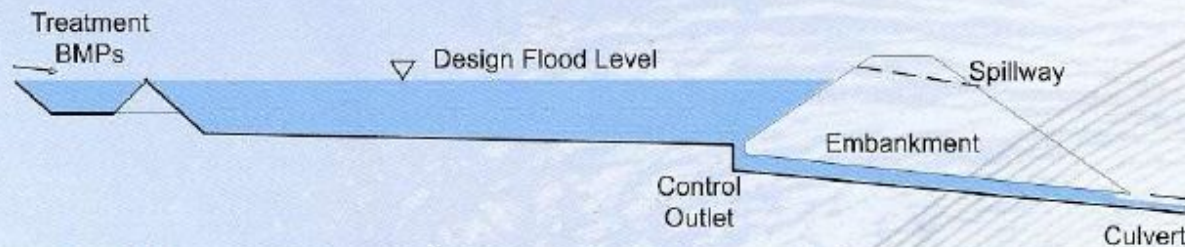


The suitability of specific SUSToM facilities depends on

- **Topography** (natural slope/depression)
- **Geology** (type of soil & its properties, i.e. porosity, infiltration & conveyance)
- **Internal drainage**
- **Sub-catchments**
- **Connection to the main drain**

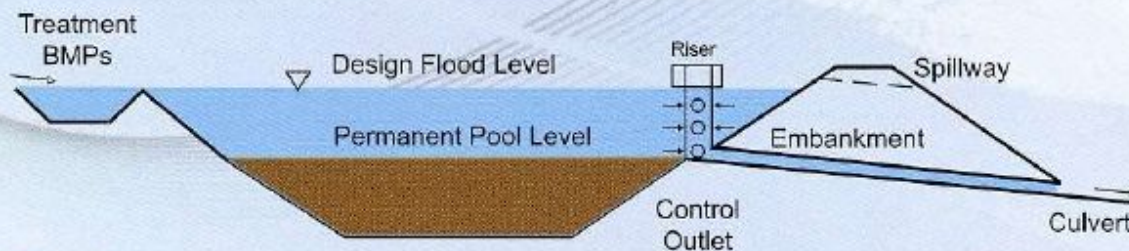
On-Site Detention

Recommended < 5 ha



Dry Ponds

Recommended 5 ha – 10 ha



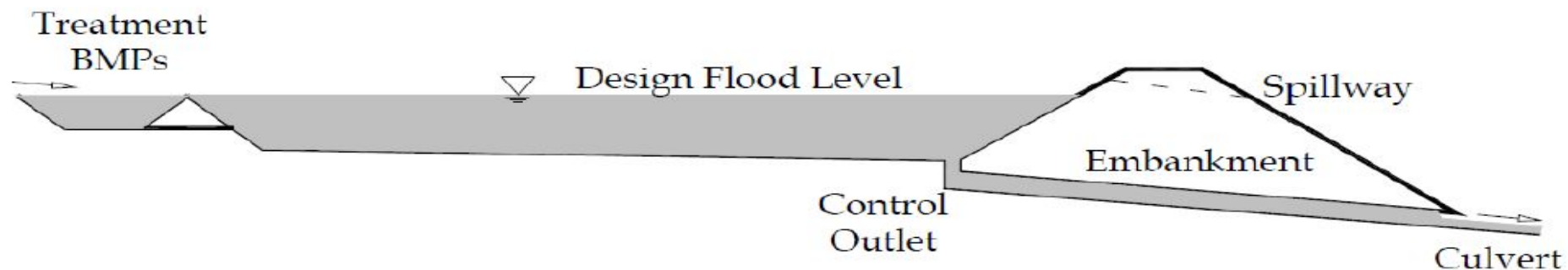
Wet Ponds

Recommended > 10 ha

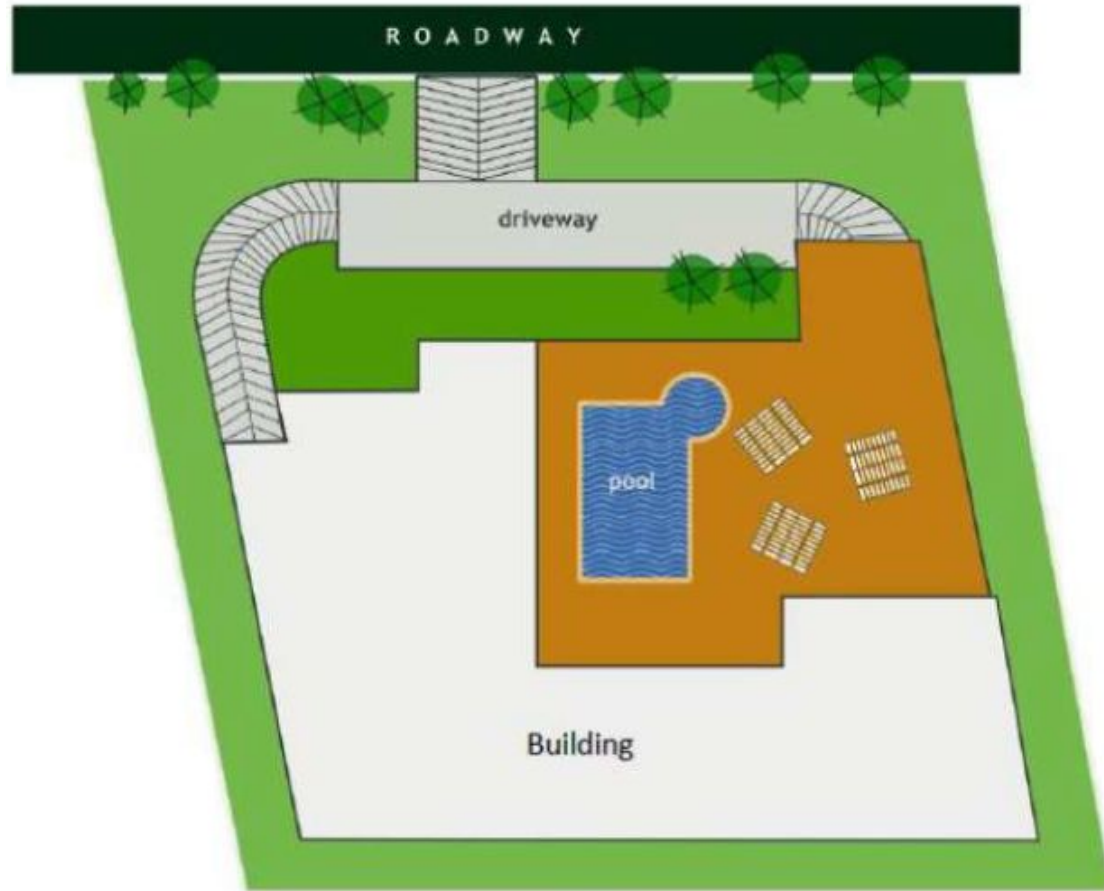
STORMWATER MANAGEMENT/ GREEN INFRASTRUCTURE



2. Detention pond reduces flood peak discharge downstream by temporary storage and gradual release using control outlet, usually ungated structure, riser or culvert, located at the base of the embankment.
3. Release Timing – Dry pond to be emptied within 12 hours while wet pond should be hours after rain ceases.



Stormwater Detention Tank System



Not to Scale

Source: On-Site Stormwater Detention Tank Systems, Technical Guide (Revision 3: Aug 2024) by Public Utilities Board, Singapore



- OSD would have to be placed at the most downstream end of the internal drainage network.
- Larger sites have greater flexibility of implementing one or more types of detention systems

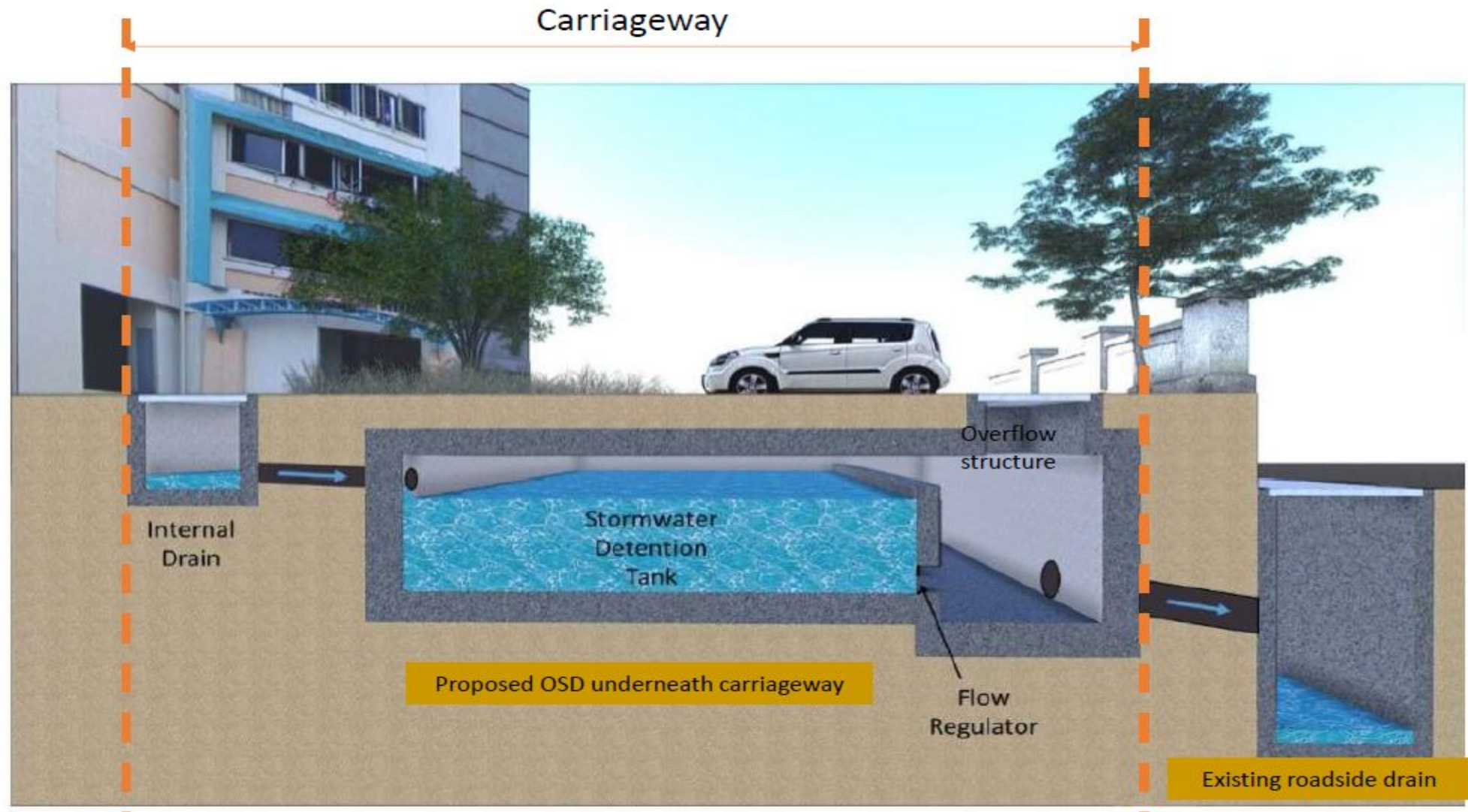
Stormwater Detention Tank System



Detention in Car-Parks: up to 150 mm depth , 20-30 min

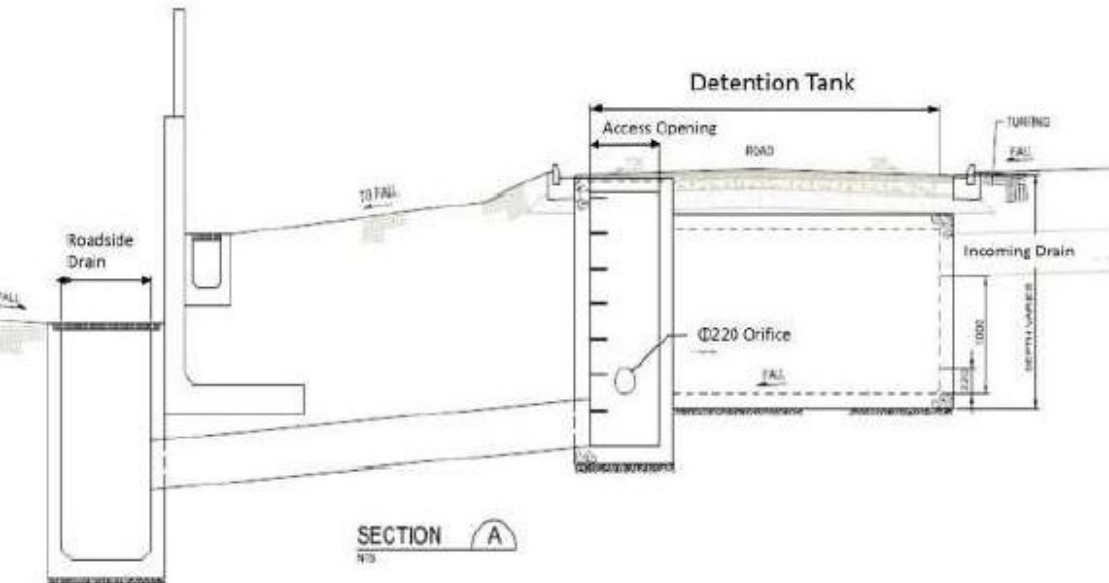
Sources: DID, Kuching, Sarawak

Stormwater Detention Tank System

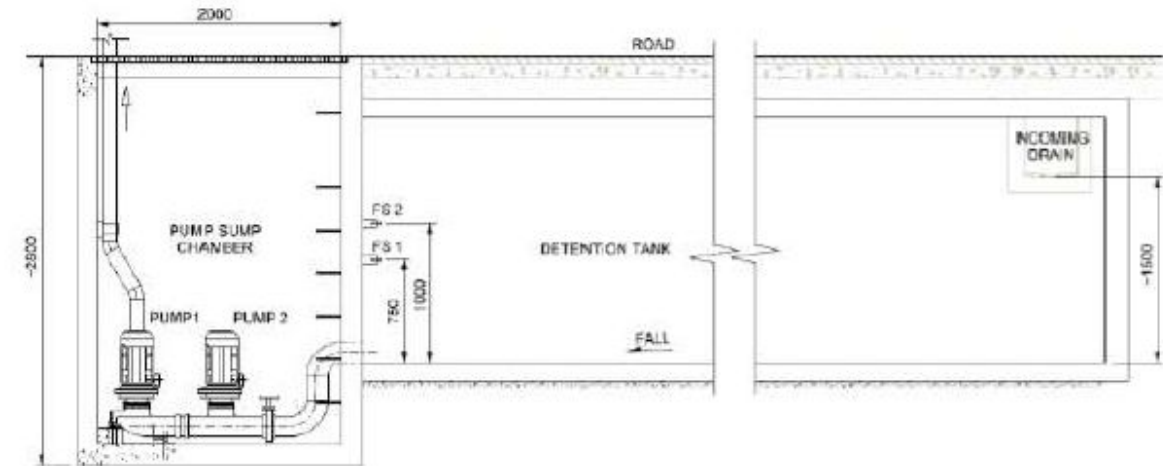


Source: On-Site Stormwater Detention Tank System, Technical Guide (Revision 1: May 2021) by Public Utilities Board, Singapore

Detention Tank Schematic Section



Gravity Discharge



Pumped Discharge

Stormwater Detention Tank System

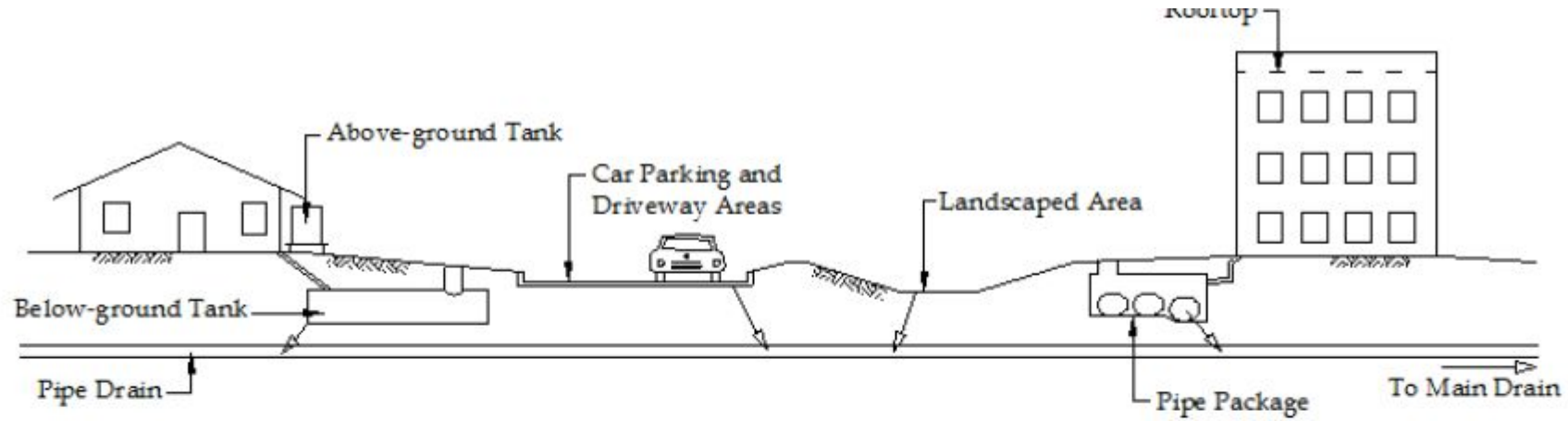


Figure 5.1: Typical OSD Storage Facilities



Stormwater Detention Tank System



Sources: DID, Kuching, Sarawak

DRY DETENTION POND

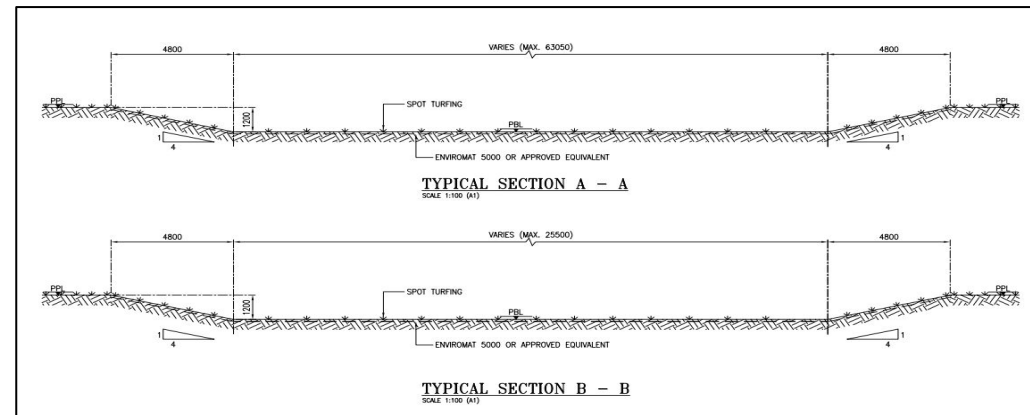


**Dry Detention Pond at SK Muara Tuang,
Samarahan**

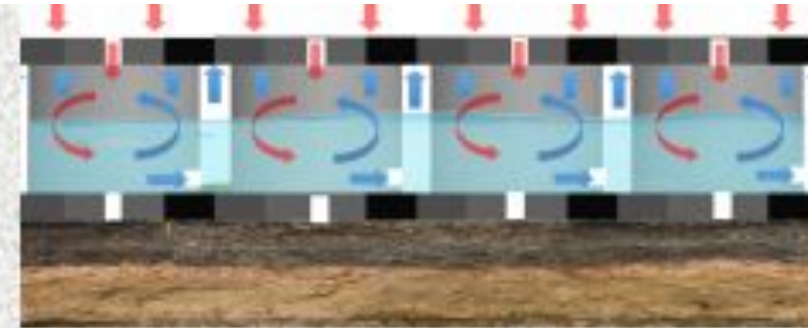
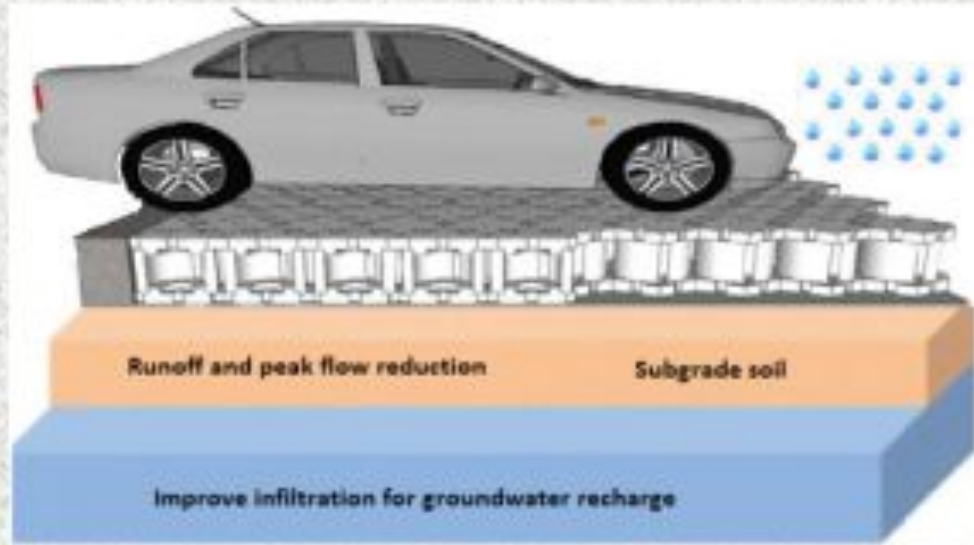


**Dry Detention Pond at Dayak Chamber Of Commerce
And Industry, Jalan Simpang Tiga**

Dry Detention Pond



Permeable Pavement with Micro-Detention Pond Storage (StormPav)



Flow of water in the micro detention pond



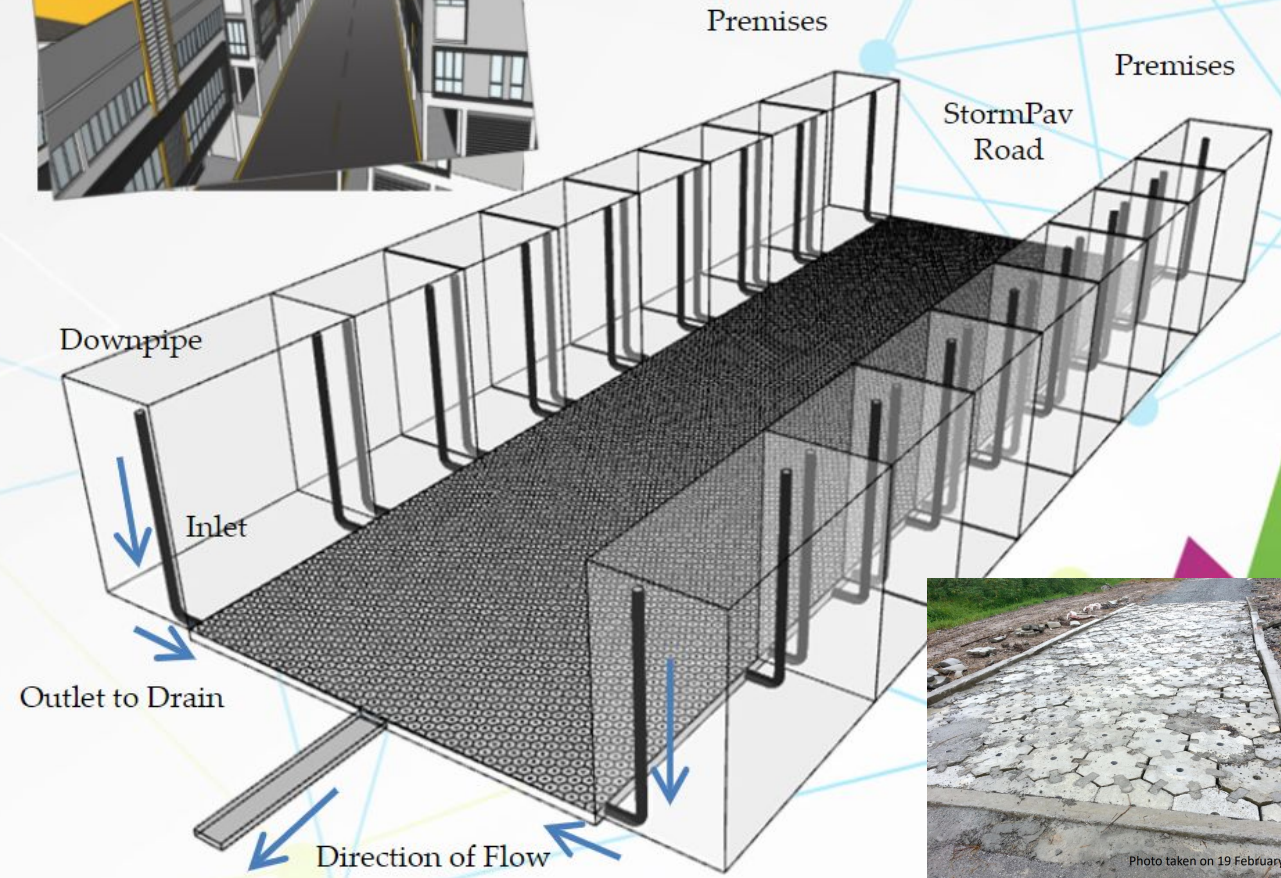
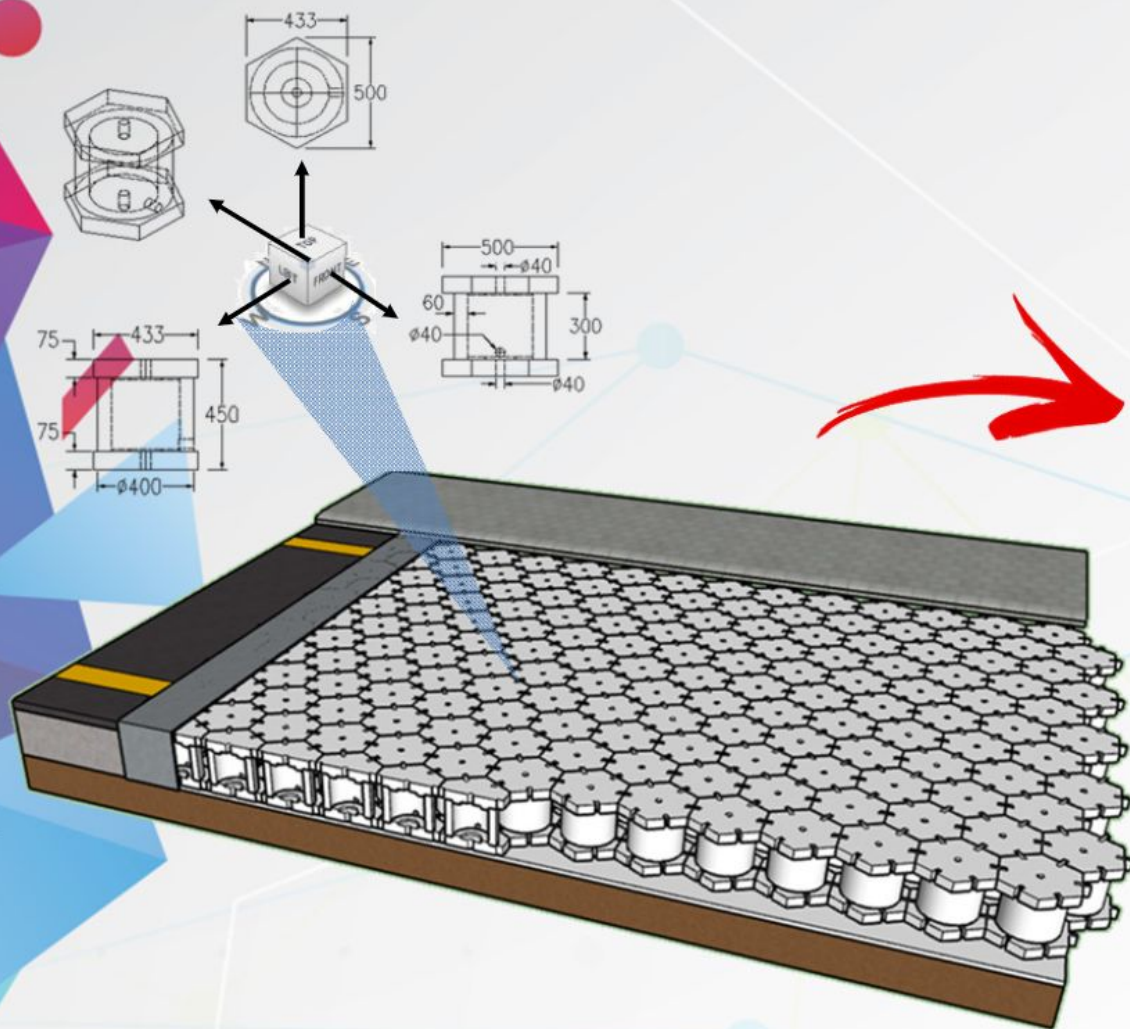
StormPav system (a) arrangement of StormPav assembled outside the laboratory



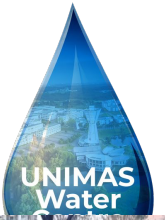
(b) StormPav precast product single unit of a hollow cylinder and cover design.



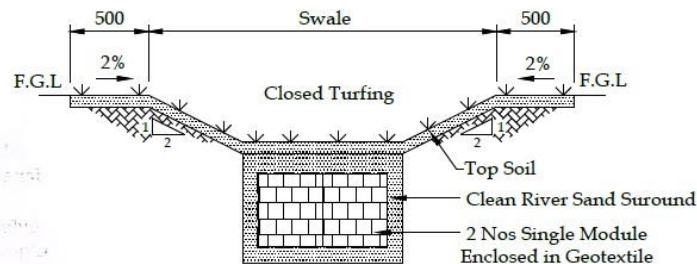
StormPav Green Pavement offers an alternative construction method for roads.



MOVA subsurface stormwater



- Control at source by promoting infiltration
- Particulate pollutant is absorbed by vegetation and porous media at the top of the module
- MOVA subsurface module is suitable for both detention and conveyance.



OSD Taman Fajar, Kota Kinabalu, Sabah, Malaysia



Kampung Haji Baki, Kuching, Sarawak, Malaysia

METHODOLOGY



Design Calculation- Two main parameters involve in the design of the stormwater drainage system is the a) **estimation of a peak runoff (Peak flood flow)** and the b) **design of suitable structure to accommodate it.**

a) Hydrology Design for Runoff Quantity Design Fundamentals using Rational Method to include as follows;

Quantity Design Fundamentals (ARI yrs- minor and major storm), refer Table 1.1, Chapter 1, MSMA

Time of Concentration $T = t_d + t_o$, refer Table 2.1 (QUDM, 2007), Chapter 2, MSMA.

Design Rainfall, i , refer Table 4.1 / Fig 5.1-5.4, HP26 for Sarawak fitting constant of i and CCF Factor Table 7.1, HP26

Peak Discharge Estimation using Rational Method, $Q = CiA/360$, C refer catchment land use to its' imperviousness and A is catchment area

b) Hydraulic Design of the Stormwater Management Facility-Detention Box design to accommodate SUSTOM FACILITY

Storage Capacity Design of SUSToM Facilities –drainage
storage using Manning's Formula, $Q=AV$ & $V=$
 $1/n(R^{2/3}S^{1/2})$, Manning's roughness coefficients Table 2.3,
MSMA

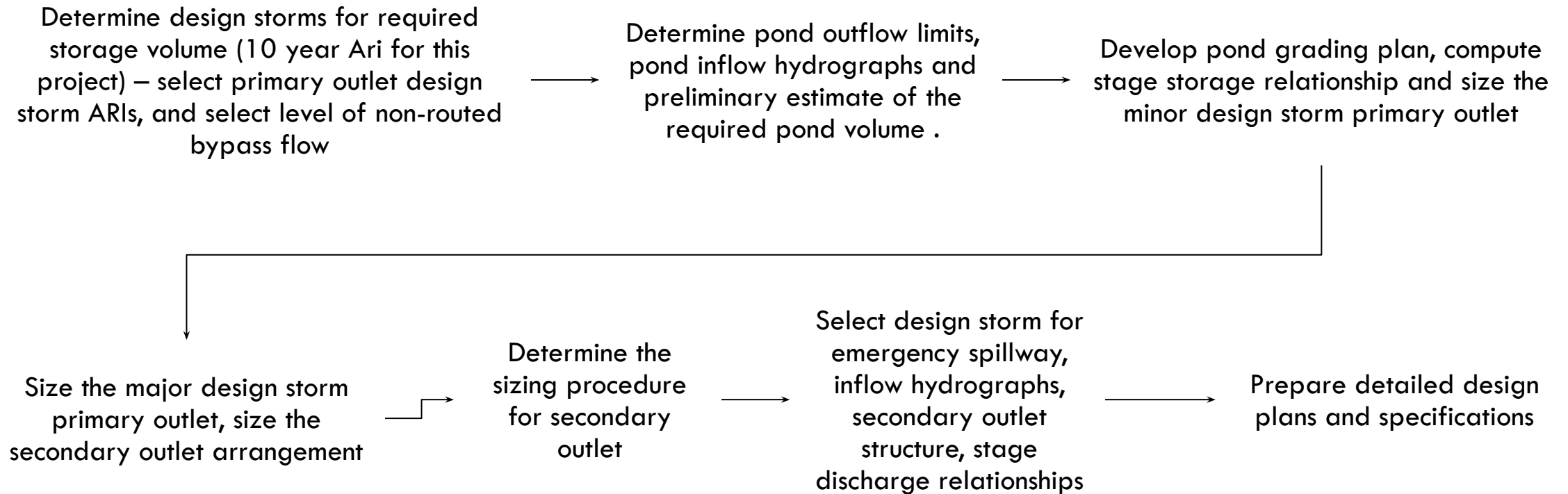
→ Select storage type- this project
used below ground storage.

↓

Determine Catchment area drain to the Detention Box drain,
Impervious and pervious area, t_c and t_{cs} , and calculate pre and
post development flows, Q_p and Q_a from t_c

→ Determine required PSD and
SSR using Equation 19.1 and
19.2, MSMA 1.

c) Hydraulic Design of the Stormwater Management Facility-Detention Pond design to accommodate a)



CASE STUDY 1: INFLUENCE OF TC ON PEAK RUNOFF

Investigates how T_c affect the design and performance of detention ponds

$$T_c = t_d + t_o$$

T_c = Time of Concentration, min

t_d = drain flow time = L/V , min

L = Drain length, m

V = Assume velocity, m/s

t_o = Overland flow time = $107.n.Lo^{1/3}/s^{0.5}$, min

Lo = overland flow path, m

n = Manning Roughness coefficient

s = slope of overland surface, %

Parameters will be extracted from the existing design reports

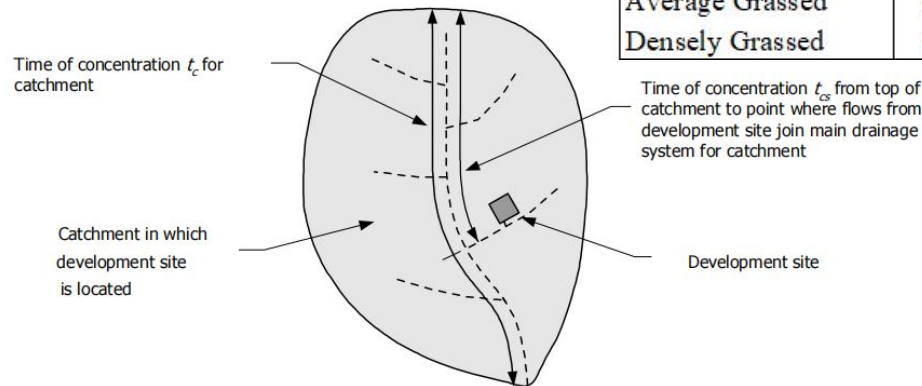
- Drain Length (m)
- Assume velocity (m/s)
- Overland Flow Path (m)
- Manning Roughness coefficient
- Slope of overland surface

Table 2.2: Values of Horton's Roughness n^* (QUDM,2007)

Land Surface	Horton's Roughness n^*
Paved	0.0150
Bare Soil	0.0275
Poorly Grassed	0.0350
Average Grassed	0.0450
Densely Grassed	0.0600

Table 2.3: Values of Manning's Roughness Coefficient (n) for Open Drains and Pipes

Drain / Pipe	Manning Roughness n
Grasses Drain	
Short Grass Cover (<150mm)	0.035
Tall Grass Cover (>150mm)	0.05
Stone Pitching	
Dressed Stone in Mortar	0.017
Random Stones in Mortar or Rubble Masonry	0.035
Rock Riprap	0.03
Brickwork	0.02
Pipe Material	
Vitri fied Clay	0.012
Spun Precast Concrete	0.013
Fibre Reinforced Cement	0.013
UPVC	0.011



CASE STUDY 1: INFLUENCE OF TC ON DEAK DI INIOEE



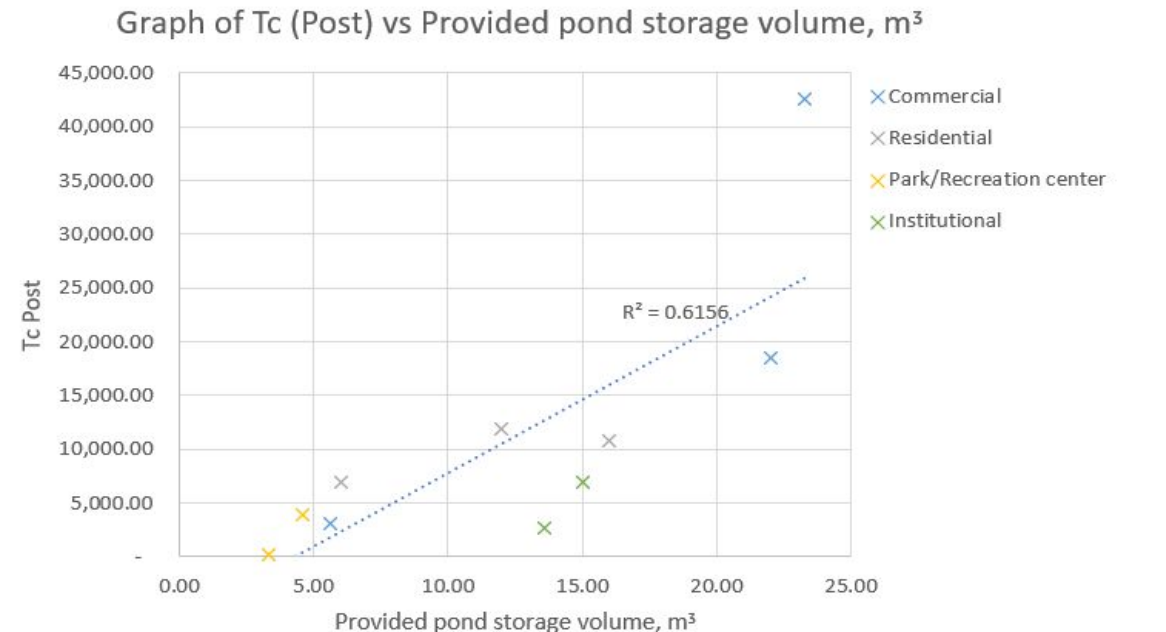
Table 4-1:
Factors Influencing Time of Concentration, Tc across Subcatchments

Catchment ID	Land Use	Lo (m)	n* (Horton)	So (%)	Ld (m)	n (Manning)	Sd (%)	to (min)	td (min)	Tc (min)
DP1	Residential	35.00	0.0150	3.33	440.00	0.013	0.0033	4.1	7.2	12
DP2	Residential	34.50	0.0450	1.10	345.00	0.015	0.0033	15.4	0.5	16
DP3	Residential	20.00	0.0150	5.00	200.00	0.013	0.0033	3.2	2.7	6
DP4	Commercial	89.04	0.0450	4.50	915.00	0.015	0.0033	15.9	5.1	21
DP5	Commercial	3.00	0.0450	1.00	250.00	0.013	0.0020	6.9	2.8	10
DP6	Commercial	395.10	0.0275	2.60	1110.90	0.013	0.0033	17.8	5.5	24
DP7	Institutional	260.00	0.0150	0.38	220.00	0.013	0.0045	12.4	1.2	14
DP8	Institutional	45.00	0.0150	2.00	200.00	0.013	0.0020	5.0	1.3	7
DP9	Park/Recreation Center	0.00	0	0	251.00	0.017	0.0020	0	3.3	4
DP10	Park/Recreation	0.00	0	0	347.00	0.017	0.0020	0	4.6	5

CASE STUDY 1: INFLUENCE OF TC ON PEAK RUNOFF

Detention Pond	Types of Development	Tc Pre	Tc Post	Estimated pond storage volume, m ³	Provided pond storage volume, m ³
DP1	Residential	22.35	7.00	10,844.41	11,948.76
DP2	Residential	20.34	16.00	9,693.90	10,827.44
DP3	Residential	22.69	6.00	5,226.25	6,880.13
DP4	Commercial	33.13	22.00	12,458.66	18,505.08
DP5	Commercial	27.23	5.60	2,162.74	3,092.10
DP6	Commercial	38.37	23.30	41,951.06	42,520.88
DP7	Institutional	27.51	13.58	641.49	2,655.00
DP8	Institutional	22.30	7.00	11,561.49	11,948.76
DP9	Park/Recreation center	12.18	3.31	93.59	140.30
DP10	Park/Recreation center	28.00	4.60	2,619.41	3,868.60

Min Tc	3.31 DP9 (Park)
Max Tc	23.30 DP6 (Commercial)
Min. Provided pond storage volume, m ³	140.30 DP9 (Park)
Max. Provided pond storage volume, m ³	42520.88 DP6 (Commercial)



CASE STUDY 1: INFLUENCE OF TC ON PEAK RUNOFF

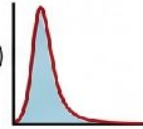
CROSS-SECTIONAL ILLUSTRATION: IMPACT OF TIME OF CONCENTRATION (T_c) ON SUSTOM DRY DETENTION POND DESIGN

Catchment Characteristics Influencing T_c



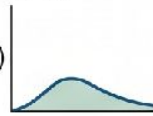
Subcatchment A (Short T_c)

Steep Slope
High Imperviousness
(e.g., Commercial Area)
Smooth Surfaces



Subcatchment B (Long T_c)

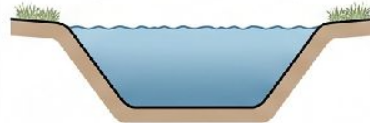
Gentle Slope
Low Imperviousness
(e.g., Park/Residential)
Rough Surfaces
(Vegetation)



Impact of T_c on Detention Pond Sizing

Pond 1

(Designed for Short T_c)
Requires **LARGER** Storage
Volume and Footprint due to
Higher Peak Discharge

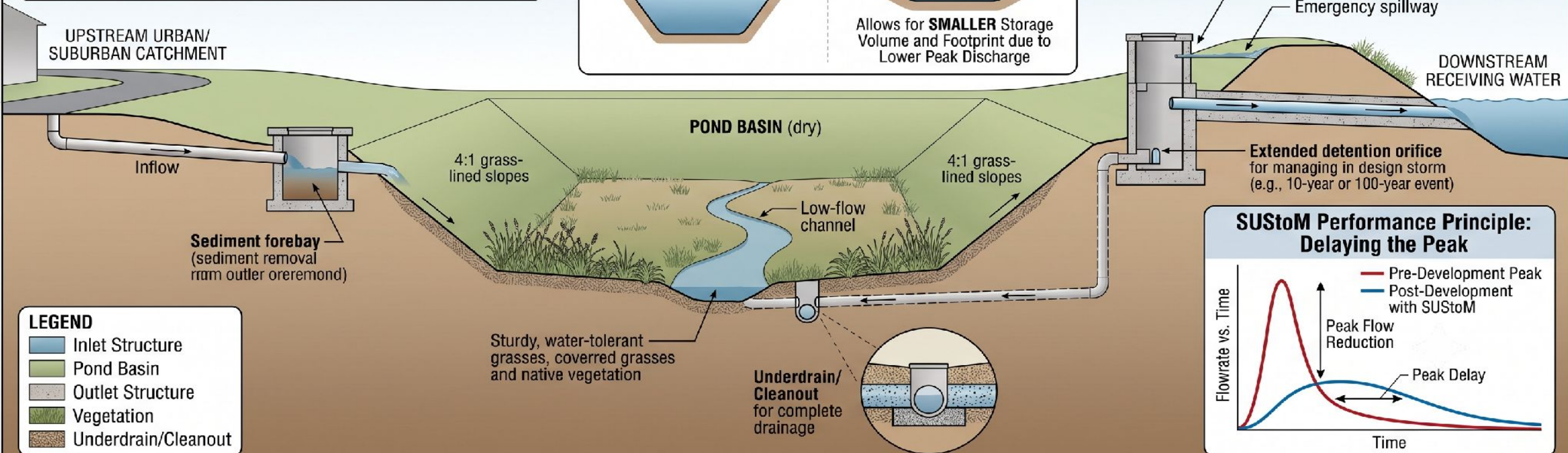


Pond 2

(Designed for Long T_c /
SUSToM Effective T_c)



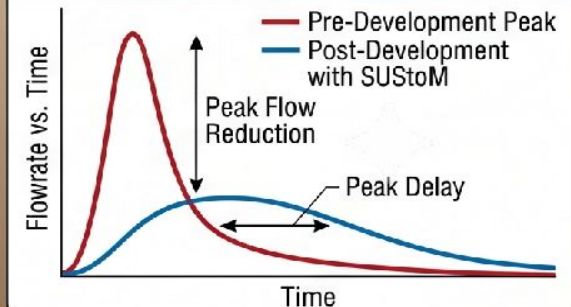
Allows for **SMALLER** Storage
Volume and Footprint due to
Lower Peak Discharge



LEGEND

- Inlet Structure
- Pond Basin
- Outlet Structure
- Vegetation
- Underdrain/Cleanout

SUSToM Performance Principle: Delaying the Peak



SUSToM FACILITY: CROSS-SECTIONAL ILLUSTRATION OF DRY DETENTION POND

Vegetated Bed and Slope 4:1



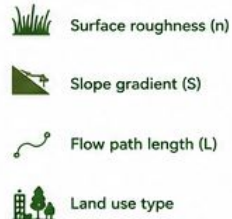
STUDY OVERVIEW (10 DRY PONDS)



Total: 10 Existing SUSToM Dry Detention Ponds

Data validated using design reports, field verification and site observations

FACTORS INFLUENCING TIME OF CONCENTRATION (T_c)



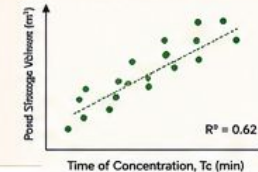
- ✓ T_c mainly influenced by these factors.
- ✓ Urban areas (commercial/residential) give shorter T_c .
- ✓ Parks / recreational areas give longer T_c .
- ✓ Accurate parameterization is critical for reliable stormwater design.

VARIATIONS IN TIME OF CONCENTRATION (T_c) ACROSS DIFFERENT SUBCATCHMENTS



KEY FINDING

Moderate correlation ($R^2 = 0.62$) between T_c and storage volume. T_c vs storage volume explains most but not all storage needs. Design must be tailored to catchment type.



IMPACT OF TIME OF CONCENTRATION (T_c) ON DESIGN AND PERFORMANCE



T_c directly affects pond sizing and performance.



Shorter T_c → faster runoff generates higher peak discharge → requires more immediate storage.



Longer T_c → inflow is spread out → larger total volume needed for effective detention.



Errors in T_c estimation → under/over-designed ponds → higher flood risk or wasted cost.

TYPICAL T_c RANGE OBSERVED (10 CASES)

Short T_c (Commercial / Residential)	5 – 15 min
Longer T_c (Institutional / Parks)	20 – 45 min

SUMMARY OF FINDINGS

- ✓ T_c varies significantly by land use and subcatchment characteristics.
- ✓ Commercial / institutional sites generally have longer T_c and larger pond volumes.
- ✓ Parks / recreational sites generally have shorter T_c and smaller volumes.
- ✓ Moderate correlation ($R^2 = 0.62$) between T_c and storage volume.
- ✓ Accurate determination of T_c is essential for optimal design and cost-effective performance.

BENEFITS OF WELL-DESIGNED DRY DETENTION PONDS



Delay peak discharge



Reduce downstream flooding



Support infiltration and water quality



Provide amenity and green space



Cost-effective and sustainable solution

LEGEND (CROSS SECTION)

- 1 Runoff Generation
 - 2 Inlet Structure
 - 3 Dry Detention Pond (Vegetated Bed)
 - 4 Outlet Control Structure
 - 5 Discharge to Downstream System
- Design Maximum Water Level
- Flow Direction



KEY MESSAGE: Accurate determination of Time of Concentration (T_c) and subcatchment T_c is critical for effective SUSToM design. By increasing the effective T_c , dry detention ponds delay peak discharge, allow runoff to be detained and released more gradually, thereby reducing peak flow and mitigating downstream flooding.

CASE STUDY 2 FACTORS INFLUENCE DRY POND & OSD

STUDY AREA OVERVIEW: SARAWAK, MALAYSIA | PROPOSED SUSTOM (SUSTAINABLE STORMWATER MANAGEMENT) FACILITIES

SITE 1: KUCHING Lot 4729 (Near Kuching Sentral)

TOTAL AREA:
15,178 m²



LAND USE:
HOUSING DEVELOPMENT



SUSToM FACILITY: UNDERGROUND TANK

SITE 2: KUCHING Lot 1405-1409 (Near Sungai Moyan)

TOTAL AREA: 22,691 m²
OPEN SPACE AREA: 2,011 m²



LAND USE:
HOUSING DEVELOPMENT



SITE 2: KUCHING Lot 1405-1409 (Near Sungai Moyan)

TOTAL AREA: 22,691 m²



LAND USE:
HOUSING DEVELOPMENT



SUSToM FACILITY: UNDERGROUND TANK

SITE 3: KOTA SAMARAHAN Lot 2938 (Near Kampung Tanjung Bako)

TOTAL AREA: 5,336.27 m²
LAND USE:
PETROL STATION



SUSToM FACILITY: UNDERGROUND TANK

SITE 5: SIBU, Lot 1970 & 2585 (5km away from Sibu Airport)

TOTAL AREA: 117,552 m²
OPEN SPACE PROVIDED:
11,820 m²



LAND USE:
HOUSING DEVELOPMENT



SUSToM FACILITY: DRY POND

SITE 4: KOTA SAMARAHAN Lot 1255 (Near IPG Samarahan)

TOTAL AREA: 103,831.12 m²
OPEN SPACE PROVIDED: 7,700 m²



LAND USE:
EDUCATIONAL INSTITUTION



SUSToM FACILITY: DRY POND

SITE 6: MIRI Lot 3119 (SMK Pujut, Miri)

TOTAL AREA: 6,288 m²



LAND USE:
EDUCATIONAL INSTITUTION



SUSToM FACILITY: UNDERGROUND TANK



CASE STUDY 2 FACTORS INFLUENCE DRY POND & OSD

No.	Studied Area	Total Area (m2)	Rainfall intensity, <u>i</u> (mm/hr)	Flow, Q (m/s ³)		Time of concentration	
			10 year ARI	<u>Qpre</u>	<u>Qpost</u>	Tc pre	Tc post
1	Lot 4729, Kuching North Land District	15,178	185.46	0.156	0.106	31.64	4.25
2	Lot 1405-1409, <u>Matang</u> Land District	22,691	203.56	0.263	0.178	24.18	7.68
3	Lot 2938, Muara <u>Tebas</u> Land District	5,336.27	222.58	0.056	0.038	29.81	3.65
4	Lot 1255, <u>Samarahan</u> Land District	103,831.12	143.18	0.978	0.433	40.97	21.25
5	Lot 1970 & 2585, <u>Seduan</u> Land District	117,552	241.47	0.924	0.639	20.00	8.00
6	Lot 3119, Miri	6,286	194.56	0.083	0.056	30.92	4.71
7	Lot 590, Kemena Land District	58,878	157.70	-	-	-	-

CASE STUDY 2 FACTORS INFLUENCE DRY POND & OSD



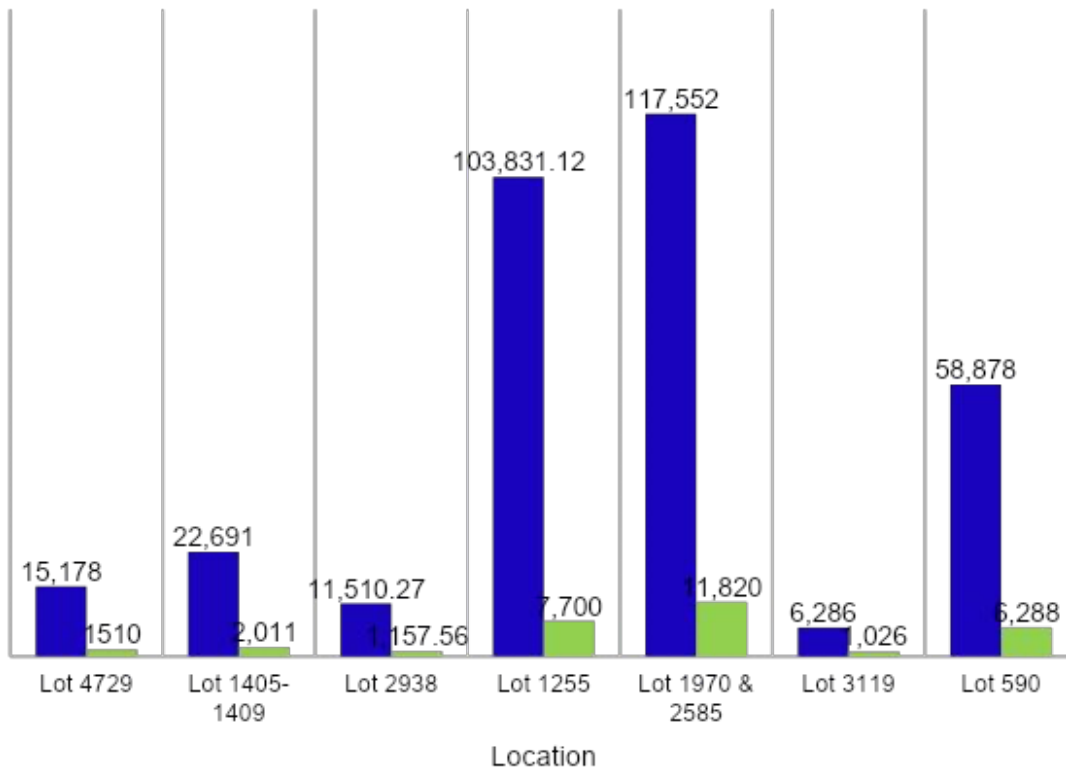
No.	Studied Area	Total Area (m ²)	Volume Required (m ³)	Volume Provided (m ³)
1	OSD Underground Tank	15,178 (1.5 ha)	1,796.64	1,800
2	OSD Underground Tank	22,691 (2.3 ha)	1,873.87	1,901
3	OSD Underground Tank	5,336.27 (0.5 ha)	559.20	573
4	Dry Detention Pond	103,831.12 (10.4 ha)	4,091.42	6,540
5	Dry Detention Pond	117,552 (11.8 ha)	9,921.00	15,390
6	OSD Underground Tank	6,286 (0.6 ha)	520.70	536
7	Direct discharge to nearby river	58,878 (5.9 ha)	0	0

****Recommended area for 5ha to 10ha for Dry Pond and OSD <5ha (SUSToM 2018, DID)**

CASE STUDY 2 FACTORS INFLUENCE DRY POND & OSD

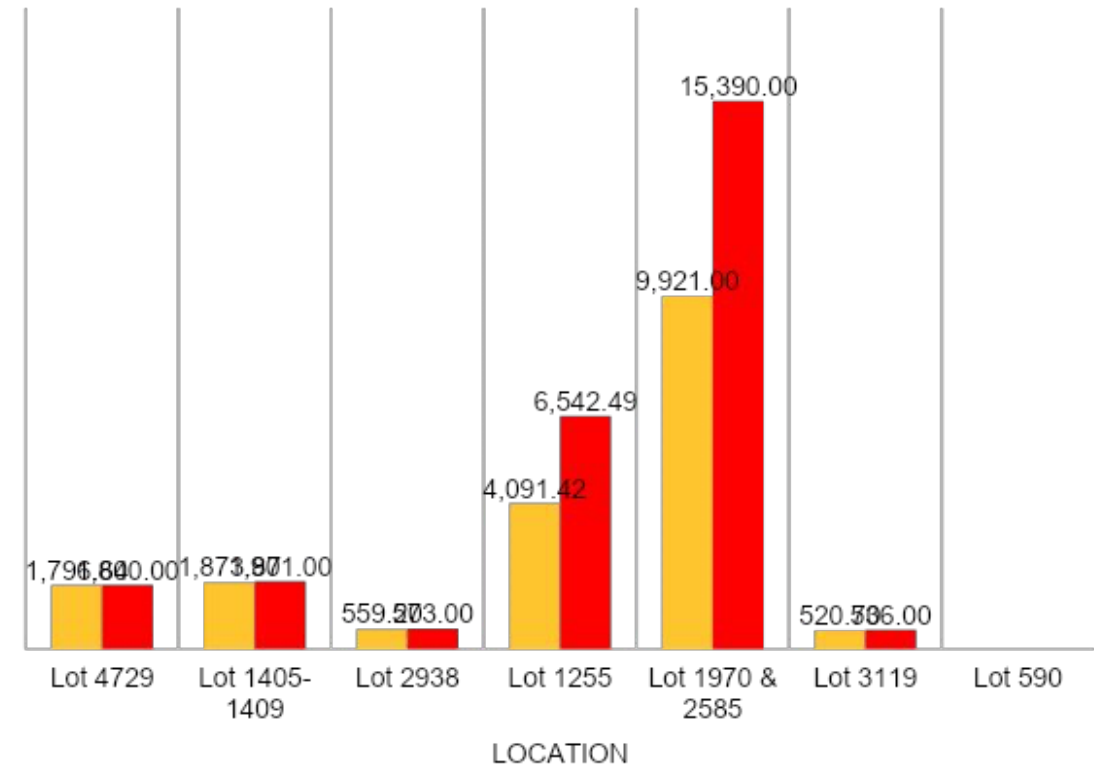
OPEN SPACE AREA OF EACH LOCATION

■ Total Area ■ Open Space Area

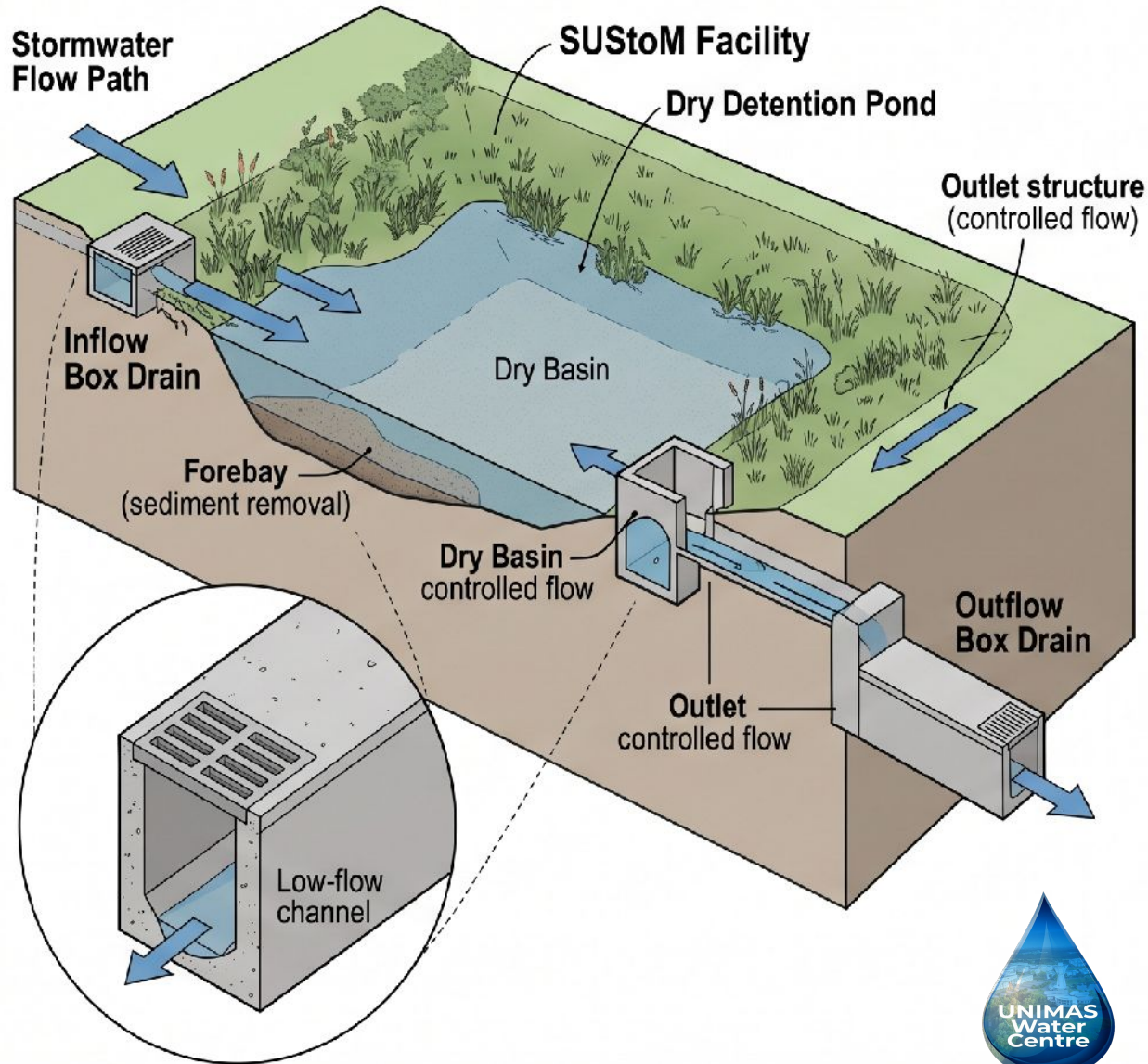


VOLUME REQUIRED

■ Volume Required (m3) ■ Volume Provided (m3)



SUSToM Facility Study Findings: Dry Detention Pond & Box Drain



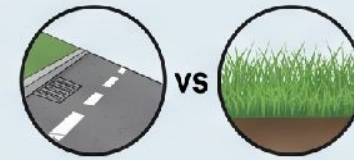
Study Overview

Performed at 6 Catchment Areas (0.5ha to 11.8ha)



Rainfall Intensity (I)

- Higher I contributes to more rainfall in a shorter time, resulting in higher peak flow (Q).
- SUSToM must provide larger storage volume for effectiveness.
- Effectiveness decreases with increasing I unless sufficient detention volume is provided.



Runoff Coefficient (C)

- Where higher C , more runoff contributes to higher peak flow (Q).
- High value of C (such 0.8-0.95 for residential or industrial building) means faster and higher volume of runoff.
- Higher impervious area will have higher C .

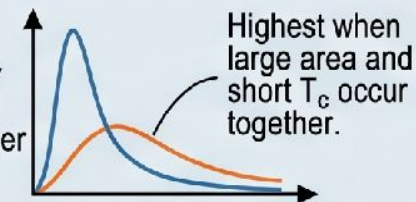


Catchment Area (A)

- Larger catchment areas generate higher total runoff volume, therefore, larger SUSToM storage is required.
- Catchment area controls the magnitude of peak flow.
- Larger areas usually have longer flow paths, which increase time of concentration (T_c).
- SUSToM effectiveness depends on adequate sizing relative to A .

Peak Flow (Q)

- A small catchment with very short T_c can produce a higher peak flow than a larger catchment with longer T_c .



Study Conclusion

- Catchment area and rainfall intensity (i) controls *how much* runoff is generated.
- Time of concentration controls *how fast* runoff reaches the outlet.
- Effective stormwater design aims to increase T_c , especially in large catchments.
- Pre- and post-development peak discharges are mainly controlled by rainfall intensity, catchment area, and runoff coefficient, with changes in runoff coefficient due to increased imperviousness being the primary factor causing higher post-development flows.

